MCE Deepwater Development 2016

Hydrate management – How to cut down cost

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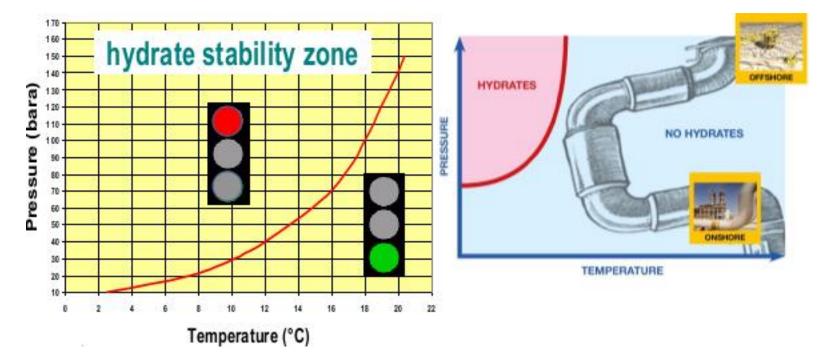




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Current hydrate management strategy

- Production outside the hydrate zone
- Requirements
 - Thermal insulation
 - Massive injection of THI* (MeOH or MEG)
 - Heating devices e;g.
 Electrical
 - Complex operating procedures e.g. Dead oil preservation





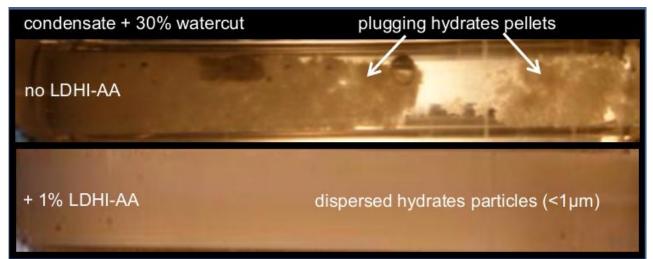
^{*:}THI = Thermodynamic Hydrate Inhibitor

AA-LDHI: a way to produce inside the hydrate zone

- AA-LDHI: Anti-Agglomerant Low Dose Hydrate Inhibitor
 - Injection dose: ~ 1% / hydrate phase to be compared with ~ 50% / water phase for THI*
- Formation of a slurry of fine hydrate particles dispersed in the suspending liquid phase (no agglomeration, no deposit formation)
- Limitation in terms of slurry viscosity

$$\mu = \mu_L \frac{1 - \phi_{hyd}}{\left(1 - \frac{\phi_{hyd}}{\phi_M}\right)^2} \quad ; \quad \phi_{hyd} < \phi_M \approx 60\%$$

*:THI = Thermodynamic Hydrate Inhibitor





Development of an in-house simulator

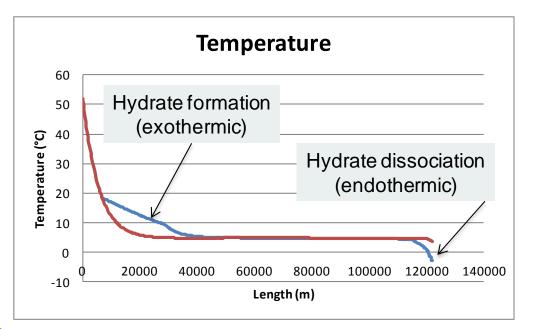
- A predictive tool to handle formation and flow of hydrate slurries
- Main hypotheses
 - Steady state 2-phase flow conditions
 - Thermodynamic equilibrium (no kinetics conservative approach)
 - Compositional calculation
 - Slurry viscosity = viscosity of a dispersed suspension
 - Exothermicity of hydrate formation considered in thermal calculations

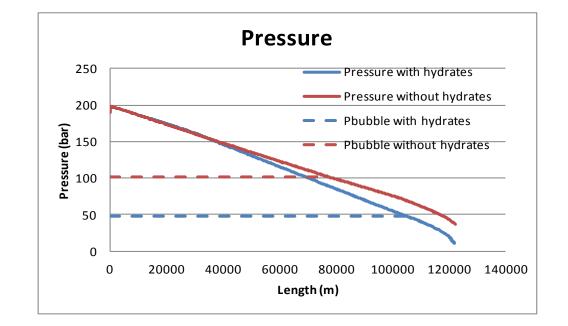


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Development of an in-house simulator

- Example
 - single liquid flow with a condensate saturated with gas at 150 bar and at WC=20%

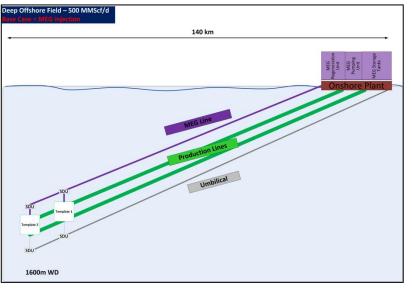


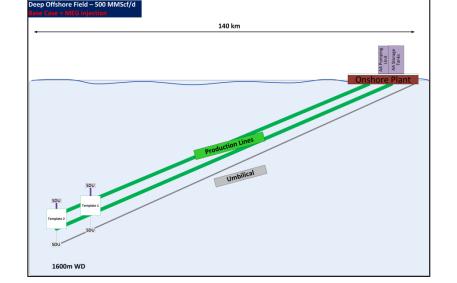




Application to subsea gas fields

- New architecture concept for gas field developments
 - 1x6" pipe for MEG transport \rightarrow AA-LDHI in existing umbilical (~1 bbl/d)
 - MEG regeneration unit at onshore





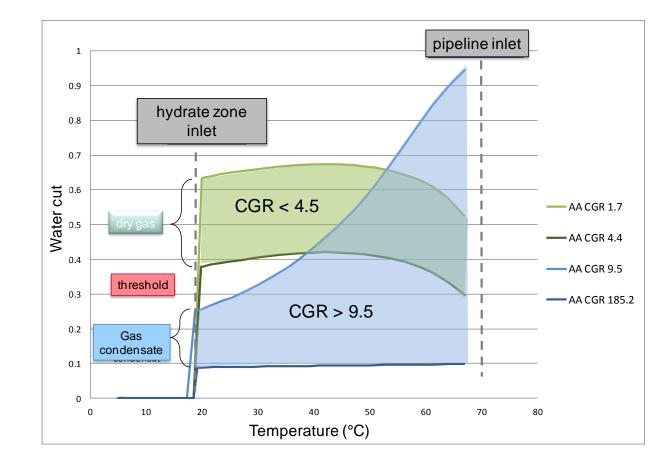
Cutting CAPEX ~ 400 M\$

- Additional possible cutting CAPEX
 - Lower liquid content \rightarrow lower hydrodynamic turndown
 - •-2 production lines \rightarrow 1 production line



Application to subsea gas fields: Operational envelop

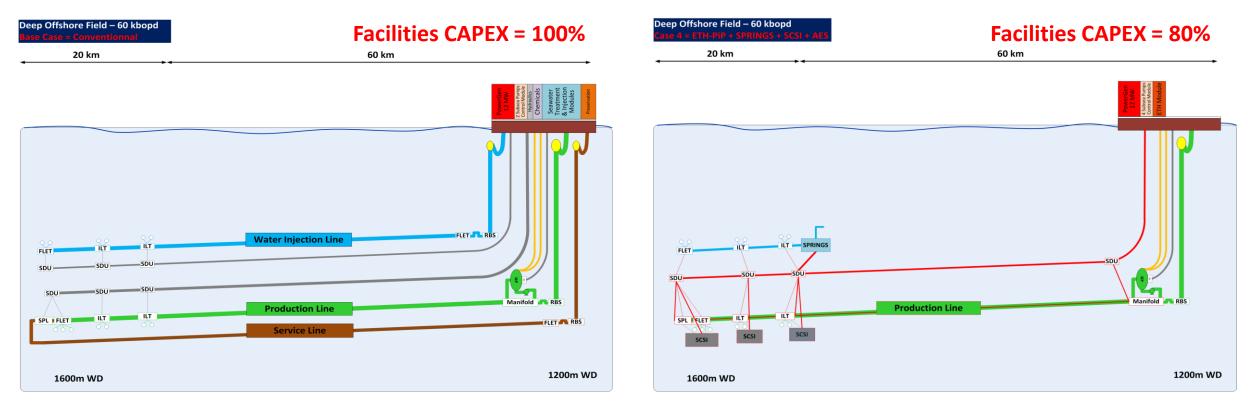
- Only condensed water is considered
 - All the water phase is transformed into hydrate
 - No salt
- Key point: WC at the entrance of the hydrate zone
- CGR is the main relevant parameter for hydrate transportability
- CGR threshold: ~ $4 10 \text{ SMm}^3/\text{Sm}^3$
 - Can vary depending on the pressure in the line
 - Might be higher in case of production of reservoir water





Application to satellite subsea oil fields

• Production line + service line \rightarrow ETH*-PiP + Subsea systems + all elec.



Adapted from L. Riviere MCEDD Pau 2016



*:ETH = Electrical Trace Heating

Application to satellite subsea oil fields

- Another gain step can be reached by replacing the 12"/18" ETH-PiP by 14" wet insulated pipe
 - CAPEX 80% → CAPEX 62% (according to L. Riviere MCEDD Pau 2016)
- Batch injection of AA-LDHI for degraded flow conditions and planned shutdowns (makes feasible subsea storage)
- Risk of hydrate formation during long unplanned shutdowns and restarts
 - Depressurization at the SSU*: may be not enough
 - Continuous injection of AA-LDHI for unplanned shutdowns management might result in high OPEX

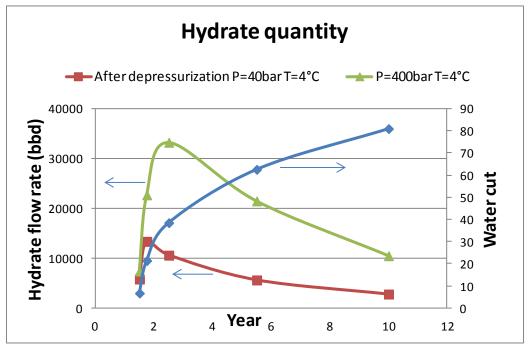


* SSU = Subsea Separation Unit

Application to satellite subsea oil fields

- A case-by-case risk assessment is required by considering:
 - Maximum quantity of hydrate that can form
 - Thermodynamic conditions
 - Limited by GOR and salinity of produced water

- Actual quantity of hydrate that can form
 - Kinetics effect



- Natural AA properties of the oil
 - May enable to drastically reduce the quantity of AA-LDHI be continuously injected

Conclusions

- Subsea gas fields
 - Large cutting CAPEX by replacing MEG with AA-LDHI
 - Can be applied to low CGR cases
- Satellite subsea oil fields
 - In addition to the simplified 'single line' architecture, AA-LDHI can offer an another significant cutting CAPEX.
 - Batch injection of AA-LDHI to manage degraded conditions and planned shutdowns
 - A case-by-case risk assessment is required for long unplanned shutdowns
 - Continuous injection of AA-LDHI may be lead to high OPEX
 - Should depend on oil properties



THANK YOU FOR LISTENING

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BACK-UP



CGR and WC definitions

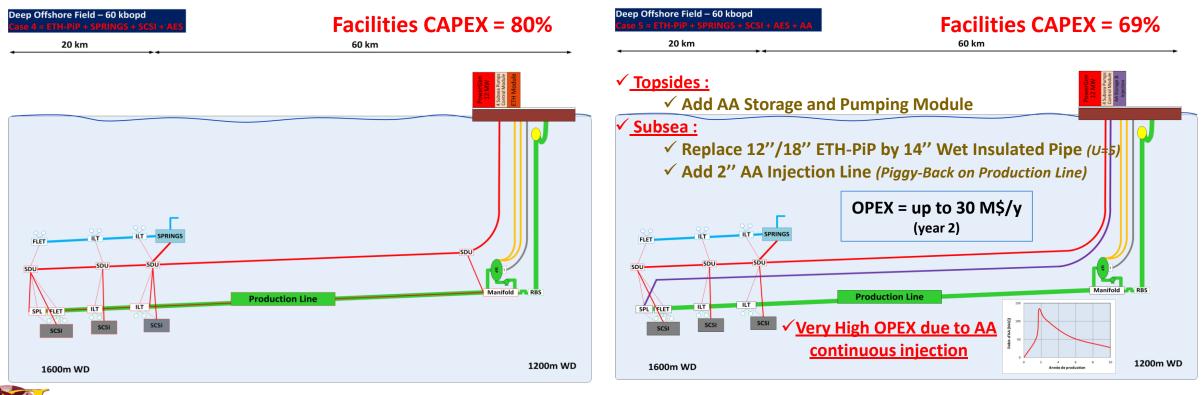
• Pseudo-process considered to calculate CGR and WC:

	1 st step	2 ^d step	3 rd step	4 th step	5 th step
P (bar)	45	60	60	45	15
т (°С)	20	6	1.5	1	1



Application to satellite subsea oil fields

• ETH-PiP \rightarrow wet insulated line + continuous AA-LDHI injection



Adapted from L. Riviere MCEDD Pau 2016